

ROENTGENS/HOUR AT D+1

410583

	Y+1		R+1		U+1	
	OBS	CALC	OBS	CALC	OBS	CALC
HOW	25	30	0	.6	8.5	9
NAN	2	7	0	<.6	.09	2
OBOE	.04	3	0	.6	0	.7
UNCLE	~0	5				
BRAVO	.5	.3				
ABLE	2	5	[50	70]		
D-E-F-G			0-.6	~10	[10-15	30-60]

BEST COPY AVAILABLE

	E+1	
	OBS	CALC
BOGALLVA	1.2	10 ⁻⁶
ELUGELAB	.14	.4
KIRINIAN	.12	1
ACMAN	.06	.6
PIIRAAI	.033	.4

HYPO (NECTAR) + 1 day
(EASY WINDS)

PARRY
ENIVETOK

10

2

30	70
30	50
30	54
10	20
10	30
10	20
10	20

RG 326 US ATOMIC ENERGY
COMMISSION F-23
Local **LANL** B-195

Gen. Records Center
Fallout Forecasting
Fast method

COPIED/DOE
LANL RC

Nectar 14 May 0620

Hods
0600

10	31	
20	31	62
30	24	86
40	34	120
50	69	189
60	40	229
70	62	291

Elmer	0	
Fred	0	
Leroy	0	
Alicia	.26	Bogalua
Janet	.08	Engelbi
Sally	0	
	.12	Bogon

Bogalua (Alicia)	700
Engelbi (Janet)	180
Amon (Sally)	27
Pogon (Wanda)	
Parry (Elmer)	0

COPIED/DOE
LANL RC

YANKEE LOCAL
FALL-OUT ANALYSIS

WINDS OF
Y 0600 5 May 54

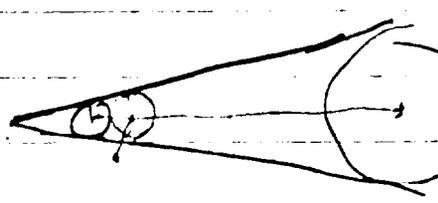
COPIED/DOE
LANL RC

		r/a							
		H	N	O	U	Br	A	B	C
12	70	1.0	1.5	1.8	2.0	2.2	1.8	1.7	1.6
11	60	1.2	1.7	2.0	2.4	2.6	2.2	2.1	2.0
10.5	50	1.0	1.6	1.9	2.3	2.6	2.2	2.1	2.0
5.7	40	1.2	2.4	2.8	-	-	-	-	2.8
4.2	30	1.9	-	2.6	-	-	2.4	2.3	2.0
3.2	20	-	-	2.2	2.5	2.7	2.2	2.1	1.9
2.7	10	-	-	-	-	-	1.7	2.2	1.4

		$\exp(-\frac{r^2}{a^2})$								conc
		H	N	O	U	Br	A	B	C	
	70	.36	.10	.040	.018	.0075	.040	.055	.078	.25
	60	.24	.06	.018	.003	.0012	.008	.012	.018	.28
	50	.36	.08	.026	.005	.0012	.008	.012	.018	.30
	40	.24	.01	.000	-	-	-	-	.000	.11
	30	.03	-	.001	-	-	.003	.005	.018	.21
	20	-	-	.008	.002	.0007	.008	.012	.027	.35
	10	-	-	-	-	-	.055	.008	.140	.51
	70	.090	.025	.0100	.045	.0019	.0100	.014	.020	
	60	.068	.017	.0050	.001	.0003	.0022	.003	.005	
	50	.109	.024	.0078	.002	.0004	.0024	.004	.005	
	40	.026	.001	.0002	-	-	.0006	.001	.004	
	30	.006	-	.0002	-	-	.0006	.001	.004	
	20	-	-	.0028	.001	.0002	.0028	.004	.009	
	10	-	-	-	-	-	.0280	.004	.072	

29.9 06.7 0258 .049 .0028 .0460 .030 .115

h	$D_0 = S_0$	S	$S_0 + S$	a_0	c	a
70	30	300	330	5.8	.008	64
60	30	270	300	5.8	.010	58
50	30	250	280	5.8	.011	54
40	10	200	210	1.9	.0023	40
30	10	124	134	1.9	.0056	25
20	10	67	77	1.9	.017	15



$(\Delta t)_{new} = \frac{1}{10} \text{ old } \Delta t$

h	$D_0 = S_0$	S	$S_0 + S$	a_0	c_1	a
70	30	30	60	5.8	.25	12
60	30	27	57	5.8	.28	11
50	30	25	55	5.8	.30	10.5
40	10	20	30	1.9	.11	5.2
30	10	12	22	1.9	.21	4.2
20	10	7	17	1.9	.35	3.2
10	10	4	14	1.9	.51	2.7

$\frac{2.01}{.13}$

calc obs

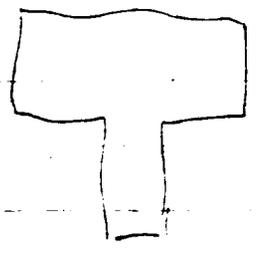
3.5

1.2

2.0

2.3

1.6



Bitini Obs 5 May @ 600 M

	0824	4.8 ✓	
1	0723	4.6 ✓	
2	0825	5 ✓	
3	0824	4.8 ✓	
4	0823	4.6 ✓	
5	0720	4 ✓	
6	0720	4 ✓	
7	0718	3.6 ✓	
8	0711	2.2 ✓	
9	0406	1.2 ✓	39
10	0205	2 ✓	} 4
12	0102	.8 ✓	
14	3405	2.1 ✓	} 43
16	3213	5.2 ✓	
18	2809	3.6 ✓	} 24
20	2914	-	
25	2323	✓	90
30	2234	✓	124
35	— 2440	est ✓	164
40	— 2640	"	200
45	(2544		244
<u>52</u>	20 ¹⁵⁸)	9	253
55	2015	9	262
60	1806		268
65	1112		280
70	0920		300
80	0945		390
90	1955		500

FCS T

COPIED/DOE
LANL RC

Bekini Obs 5 May 1500 M.

	0713
1	0715
2	0819
3	0822
4	0920
5	18
6	16
7	1012
8	1110
9	1209
10	1409
12	1806
14	2104
16	2305
18	2410
20	2609
25	2528
30	2637
35	—
40	—
45	2757
50	2650
55	2812
60	1726
65	1432
70	1440
71	1138

COPIED/DOE
LANL RC

Forecast.
Bikini 05/0610 M May
made 05/0200 M (Fox)

0 07 20
2 06 25
4 07 25
6 08 28
8 08 25
10 06 15
12 04 08
14 36 01
16 31 10
18 30 15
20 26 15
25 23 25
30 22 30
35 22 40
40 24 55
45 24 50
50 20 40
55 20 15
60 18 06
65 11 12
70 09 20
80 09 45
90 09 55

COPIED/DOE
LANL RC

Bikini Obs May 05/0900M

0516

2 0725

4 0722

6 0920

8 0411

10 3202

12 2902

14 3508

16 2406

18 3313

20 2609

25 2535

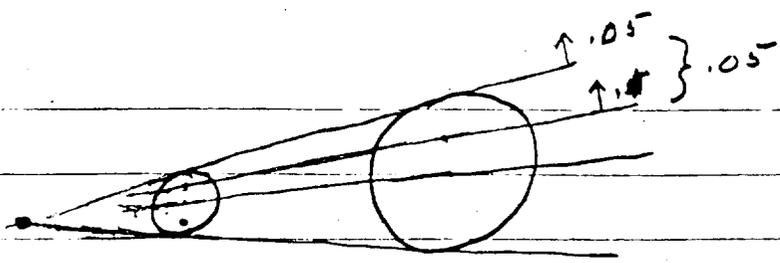
30 2416

35 2614

40 2625

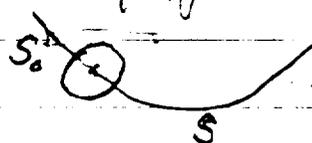
43 2651

49 2639



The problem of local heavy fall-out is primarily one of adapting the method to short distances, not much greater than the height of the cloud itself.

The distance travelled by a hydograph particle before reaching ground is calculated as $S_0 + S$, and the size, as

$$a_0 \frac{S_0 + S}{S_0}$$


where S was $\Sigma W \Delta t$ and S_0 was finally taken as equal to D_0 . If we rule out cases where the hydograph comes back over ground zero, then a small R can be achieved only by a reduction of Δt , which

requires ① an emphasis on large particles

② a need to allow for the distance of descent. It is probably reasonable to write

$$a^2 = h^2 + a_0^2 \left(\frac{S_0 + \Sigma W \Delta t}{S_0} \right)^2$$

$$= h^2 + a_0^2 \left(1 + \frac{\Sigma W \Delta t}{S_0} \right)^2$$

COPIED/DOE
LANL RC

$$= h^2 + a_0^2 \left(\frac{\Sigma W \Delta t}{S_0} \right)^2 \left[1 + \frac{2 S_0}{\Sigma W \Delta t} + \dots \right]$$

A	15.5	41	8.1	-8.0	1		
B	16	41.3	7.6	-7.5	1.3	-3.8	.6
C	17.5	41.8	6.3	-5.6	1.8	-2.5	9
→ D	23	41.2		- .5	1.2		
→ E	24.5	41.4		+ .5	1.4		
→ F	24.8	41.5		1.3	1.5		
→ G	25.5	41.1		2.0	1.1		
H	32.5	37.3	9.3	+ 9	-2.7	4.5	-1.4
L	33.5	34					
N	34	31	13.0	9.5	-9	4.8	-4.5
O	24.8	30.4	9.6	1.3	-9.6	.6	-4.8
T	22.5	29.7					
U	20.5	29.6	10.8	-3	-10.4		
Z	14	33.4	11.6	-9.5	-6.6	-4.6	-3.3
B	13.3	34.2					
	23.5	40					

BRAVO LOCAL - FAST METHOD

	S_0	S	S_0+S	p	G_0	Br	U	N	H	F
70	30	31	61		5.8	23.6	23	19.3	13.1	10.6
60	30	27	57		5.8	26.6	25	19.2	13.2	13.2
50	30	24	54		5.8	26.6	24.3	18✓	12✓	13✓
40	10	17	27		1.9	19✓	18	15.6	9.6	5.7
30	10	9.7	20		1.9	12✓	12.4✓	15✓	10.8✓	2.3✓
20	10	15	15		1.9	7.9✓	10.8✓	17.2	14.5	6.8✓
10	10	2	12		1.9	8.2✓	12.7	20	17	9.2

	p				
70	2.0	4.1✓	4.0✓	3.3✓	2.3✓
	1.9	4.6	4.3	3.3	2.3
	1.8	4.6	4.2	3.1	2.1
	2.7	10	-	-	5.1
	2.0	6.4	6.6	-	5.7
	1.5	4.2	5.7	-	-
	1.2	4.3	6.7	-	-

COPIED/DOE
IANL RC

	Br	U	N	H	F
	.004	.005	.017	.070	.115
	.001	.002	.013	.064	.064
	.001	.002	.016	.080	.070
	-	-	-	.004	.038
	-	-	-	-	.180
	-	-	-	-	.001
	-	-	-	-	-
	.006	.009	.046	.218	.468
X100	.6	.9	4.6	22	47
Obs	1.0	1.0	9.0	24	55

COPIED/DOE
LANL RC

R

$$G = \frac{S_0 + S}{S_0} G_0$$

$$C = 30$$

<u>h</u>	<u>D₀ = S₀</u>	<u>S</u>	<u>S₀ + S</u>	<u>a₀</u>	<u>a</u>	
70	30	28	50	5.8	75	9.7
60	30	16	46	5.8	86	8.9
50	30	14	44	5.8	94	8.5
40	10	12	22	1.9	18	4.2
30	10	6	16	1.9	27	3.1
20	10	4	14	1.9	35	2.7
10	10	1	11	1.9	110	2.1

300

Summary of results

COPIED/DOE
LANL RC

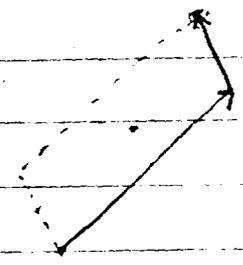
ROMEO WIND OBS

0600
27 Mar 54

06	04	2	} 2.8
2	07	2.8	
4	06	2.2	
6	04	1	
8	17	1.6	
10	18	1.6	8.8 $\times \frac{1}{10}$
12	15	2	
14	10	2	
16	09	3	³⁰
18	10	3.4	
20	10	20	39
25	17	14	
30	22	08	61
35	18	18	
40	20	36	115
45	30	05	
50	14	15	135
55	27	15	
60	27	13	163
65	32	10	
[67]	08	22	
70	09	30	203
80	09	90	
90	09	110	

$$S = \sum WAt$$

$$\frac{S_0 + S}{S_0} = \frac{S_0 + \sum WAt}{S_0}$$



COPIED/DOE
LANL RC

ROMEO

Date 27 Mar. 1954 Taken at Time 0600 L Local Observation Time 0600 L

Clouds lower 2/8 CU Base 2500 Tops 5,000 Middle None Base _____
3/8 of Cirrus Stratus Visibility 15 Miles

Sea Level Pressure 1012.4 Mb Wind direction 040 degrees Velocity 10 Kts

Surface temp 80 °F Dew Point 72 °F Humidity 77 % Vapor pressure .783

Local weather Partly Cloudy Remarks No Showers Observed

Latest winds aloft taken on Curtiss Position Bikini Time 0600

ALTITUDE	DEGREES	KNOTS	PRESSURE	TEMP	DEW POINT	R H
Surface	040	10	1012.4	80 °C	72 °C	77 Ft
1,000 Ft	:	:	:	:	:	:
1,500	:	:	:	:	:	:
2,000	070	14	:	21.5	18.2	79
3,000	:	:	:	:	:	:
4,000	060	11	:	17.8	14.0	76
5,000	:	:	:	:	:	:
6,000	080	05	:	14.0	8.0	58
6 900	:	:	:	12.5	4.0	44
8,000	170	08	:	14.8	-77	21
9,000	:	:	:	:	:	:
10,000	180	08	:	13.0	:	:
12,000	150	10	:	8.8	:	:
14,000	100	10	:	5.2	:	:
16,000	090	15	:	1.1	:	:
18,000	100	17	:	-3.5	:	:
20,000	100	20	:	-7.0	:	:
25,000	170	14	:	-14.2	:	:
30,000	220	08	:	-27.0	-35.0	46
35,000	180	18	:	-39.5	:	:
40,000	200	36	:	-52.5	:	:
45,000	300	05	:	-64.3	:	:
50,000	140	15	:	-75.0	:	:
55,000	270	15	:	-82.2	:	:
60,000	270	13	:	-77.2	:	:
65,000	320	10	:	-70.5	:	:
67 000	080	22	:	-66.3	:	:
75,000	:	:	:	:	:	:
80,000	:	:	:	:	:	:
85,000	:	:	:	:	:	:
90,000	:	:	:	:	:	:
95,000	:	:	:	:	:	:
100,000	:	:	:	:	:	:
105,000	:	:	:	:	:	:
110,000	:	:	:	:	:	:
115,000	:	:	:	:	:	:
120,000	:	:	:	:	:	:

COPIED/DOE
LANL RC

HYPOTHESIS TESTING

$$u = \frac{S_0 + S_1}{S_0} = \frac{5.0 + 5}{10.2}$$

Using EASY DATA.

h.	$D_0 = S_0$	S	$S_0 + S$	σ_0	σ	C
70	30	21	51	5.8	9.8	.35
60	30	18	48	5.8	9.2	.31
50	30	15	45	5.8	8.6	.44
40	10	9.8	20	1.9	3.85	.25
30	10	4.7	14.7	1.9	2.8	.46
20	10	2.6	12.6	1.9	2.4	.63
10	10	1.8	11.8	1.9	2.3	.85

$$5.8/30 = 0.193$$

$$1.9/10 = 0.19$$

FRED	.23	5	.03	.3
ELMER	.62	14	.15	.3
YVONNE	2.1	60	.76	
JANET	2.7		.93	
ALICE	.93			

X'10+?

EASY

$$\hat{a}_0 = \frac{D_0}{S_0}$$

$$a = \frac{S_0 + S}{S_0} \times \hat{a}_0$$

h	$D_0 = S_0$	S	$S_0 + S$	\hat{a}_0	a
70	$\frac{30}{4.62} = 6.5$	18	24.5	1.25	4.7
60	6.5	15	21.5	1.25	4.1
→ 50	6.5	9.8	16.3	1.25	3.1
40	2.2	4.7	6.9	.48	1.5
30	2.2	2.6	4.8	.48	1.2
20	2.2	1.8	4.0	.48	0.97

$$\frac{1.25}{6.5} = 0.192$$

$$\frac{.48}{2.2} = 0.218$$

Flora	.38	1.1	.140
Janet	1.2		
Lucy	.96	1.0	.120
Sally	.55	.5	.06
Wilma	.39	.3	.033
Yvonne	.09	.04	.005
Alice	—	10000	1.2

(60) E + 9 hr H + 10 hr
 Solution E = 28 hr

EASY

21 APRIL 1951 0600

Ratio 59/3000

Plot knots
1/2 scale

Sfc		knots (0.9 for 2000 ft)	
2	06	6.9	
4	08	4.8	
6	16	2.9	
8	15	2.0	
10	07	2.8	10.4 18
12	12	0.8	
14	21	1.2	
16	28	2.9	
18	33	1.6	
20	31	1.2	25.6 26
25	295	6.0	
30	27	15	46.6 47
35	28	23	
40	28	28	97.6 98
45	265	31	
50	260	25	153.6 159
55	330	13	
60	330	13	179.6 180
70	090	30	21.0

WEATHER CONDITIONS

21 APRIL (M) 1951

SURFACE

0629 (M)

2/10 Cumulus at 2000 feet (est)
 8/10 Cirrostratus at 30,000 feet (est)
 Wind ENE 9 knots
 Visibility 12 miles plus
 Pressure 1010.2 mb
 Temperature 80.4° F
 Dew Point 73.0° F
 Relative Humidity 70%

UPPER AIR

0600 (M):

<u>LEVEL (ft)</u>	<u>Wind (kts)</u>	<u>Temp (°C)</u>	<u>Dew Pt (°C)</u>
SFC.	050/14	26.2	22.5
2000	070/18	21.2	18.5
4000	080/12	17.5	14.3
6000	160/06	14.5	9.8
8000	150/05	11.2	0.0
10,000	070/07	10.0	-9.2
12,000	120/02	10.0	M*
14,000	210/03	5.2	M
16,000	280/06	0.9	M
18,000	330/04	-2.9	M
20,000	310/03	-5.7	M
22,000	290/04	-9.1	M
24,000	300/07	-14.2	M
26,000	290/14	-20.0	M
28,000	270/13	-24.9	M
30,000	260/17	-28.0	M
32,000	290/21	-33.5	M
34,000	260/21	-38.0	M
36,000	270/27	-41.5	M
38,000	270/28	-46.7	M
40,000	280/28	-50.0	M
42,000	270/32	-55.0	M
44,000	260/32	-60.0	M
46,000	260/26	-65.7	M
48,000	260/23	-68.5	M
50,000	270/24	-70.8	M
52,000	290/20	-73.9	M
54,000	340/32	-76.2	M
55,000	350/13		
* Missing			
60,000	330/13		
70,000	090/30		

U FALL-OUT ANALYSIS

0600 Run.

9/r

5
x
2
2.10

	H	N	Q	G	D	A
70	.23	55.065	04	.32	26	.084
60	08	02	004	04	03	002
50	12	025	01	06	03	003
40	02	—	—	01	—	—
30	07	—	—	.26	.13	—
20	—	—	—	.55	1.00	.003
10	—	—	—	.02	.30	.045

7A	3.9	9.31.1	.68	5.5	4.4	1.4
60	1.9	.5	.01	1.0	.8	.05
50	3.0	.6	02	1.5	.7	.07
40	.2	—	—	.1	—	—
30	.1	—	—	4.4	2.2	—
20	—	—	—	19.4	35.0	.10
10	—	—	—	1.1	16.5	2.4
	<u>9.1</u>	<u>10.4</u>	<u>.71</u>	<u>33.0</u>	<u>59.6</u>	<u>4.02</u>
		2.2				

COPIED/DOE
LANL RC

V Run 0600 26 Apr 54

$$a_f = \frac{S_0 + S}{S_0} a_0 \quad c$$

Eff.		h	D ₀ = S ₀	S	S ₀ + S	a ₀	a	
1		70	30	42	72	5.8	14	(17)
2	065 08	60	30	32	62	5.8	12	(21)
3		50	30	30	60	5.8	11.5	(21)
4	090 07.2	40	10	23	33	1.9	6.2	(19)
5		30	10	14	24	1.9	4.6	(15)
6	105 07.5	20	10	7	17	1.9	3.2	(3)
7		10	10	3.5	13.5	1.9	2.6	(5)
8	125 07.0							
9								

10	115	05.5	35.2 35
12	350	1.6	
14	360	2.4	
16	240	10	34
18	290	5.6	
20	260	15	69.8 70
25	200	33	
30	250	40	143
35	240	44	
40	250	40	227
45	250	40	
50	260	28	295
55	220	09	
60	180	15	319
65	110	20	
70	90	80	419

	S	r	30	60	p	λ	
10	4	22	10	2	1.40	∞	
20	6	23	10	2	1.60	∞	
30	9	21	10	2	1.90	∞	
40	17	17.5	10	2	2.70	10	
50	24.5	18	30	6	1.82	3	.02
60	27	15.5	30	6	1.90	2.6	.045
70	31	14.5	30	6	2.04	2.7	.06

.125

x 30 = 4 r/hr

@ D+1 days

UNION

Date 26 APRIL 1954 Time 0610 L Local Observation Time 0600 L

Clouds lower 2/10 CU SC Base 1800 Tops 3500 Middle 1/10 SC Base 12000

FEW VERY THIN CI Visibility 8 Miles

Sea Level Pressure 1007.4 Mb Wind direction 062 degrees Velocity 18 Kts

Surface temp 81 °F Dew Point 76 °F Humidity 86 % Vapor pressure 1.056

Local weather PARTLY CLOUDY Remarks NO INDUCED SHOWER ACTIVITY OBSERVE

Latest winds aloft taken on CURTISS Position BIKINI Time 0600 L

ALTITUDE	DEGREES	KNOTS	PRESSURE	TEMP	DEW POINT	REL. HUMIDITY
Surface	050	: 17	: 1006	: 26.8°C	: 24.2 °C	: 81 %
1,000 Ft	060	: 21	: 979	: 24.8	: 21.7	: 78
1,500	070	: 19	: 958	: 23.3	: 20.3	: 79
2,000	080	: 18	: 942	: 22.0	: 19.4	: 83
3,000	090	: 17	: 908	: 19.4	: 17.1	: 85
4,000	090	: 18	: 877	: 17.1	: 15.0	: 85
5,000	100	: 19	: 846	: 16.2	: 14.2	: 68
6,000	110	: 18	: 817	: 16.3	: 09.8	: 30
7,000	120	: 18	: 788	: 15.9	: -02.2	: 45
8,000	130	: 17	: 760	: 13.8	: 00.0	: 70
9,000	120	: 16	: 733	: 11.2	: 04.5	: 57
10,000	110	: 12	: 707	: 09.9	: 01.8	: 41
12,000	350	: 04	: 655	: 05.8	: -05.4	: 62
14,000	360	: 06	: 608	: 03.5	: -06.7	: 50
16,000	240	: 25	: 563	: -01.2	: -11.7	: 45
18,000	290	: 14	: 522	: -06.0	: -15.5	: 56
20,000	260	: 15	: 483	: -09.0	: -16.3	: 63
25,000	200	: 33	: 397	: -17.9	: -23.5	: 62
30,000	250	: 40	: 322	: -26.0	: MB	:
35,000	240	: 44	: 259	: -37.8	: MB	:
40,000	250	: 40	: 207	: -49.5	: M	:
45,000	250	: 40	: 157	: -61.4	: M	:
50,000	260	: 28	: 123	: -73.5	: M	:
55,000	220	: 09	: 097	: -77.5	: M	:
60,000 (57000)	180	: 15	: 074	: -79.8	: M	:
65,000	:	:	: 057	: -67.7	: M	:
70,000	:	:	:	:	:	:
75,000	:	:	:	:	:	:
80,000	COPIED/DOE LANL RC	:	:	:	:	:
85,000	:	:	:	:	:	:
90,000	:	:	:	:	:	:
95,000	:	:	:	:	:	: