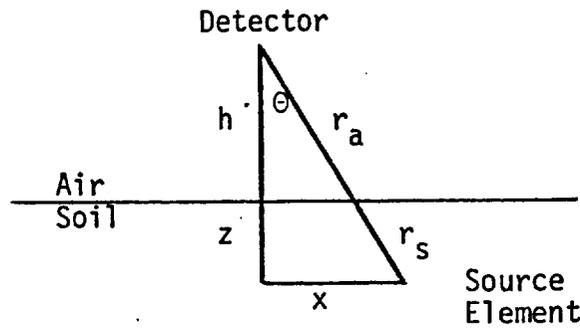


IMP CONVERSION FACTOR DERIVATION

410161



Unscattered flux at height h given by

$$\phi = \int_0^{\infty} \int_0^{\infty} \frac{S_v}{4\pi r^2} \exp\left\{-\left[\mu/\rho\right)_a \rho_a r_a + \mu/\rho\right)_s \rho_s r_s\right\} 2\pi x dx dz \quad (1)$$

where

$$S_v = \text{activity per unit volume } \left(\frac{\gamma/\text{sec}}{\text{cm}^3}\right)$$

$$r = r_a + r_s$$

$$\mu/\rho)_a, \mu/\rho)_s = \text{air and soil mass attenuation coefficients} \\ \left(\frac{\text{cm}^2}{\text{g}}\right)$$

$$\rho_a, \rho_s = \text{air and soil density (g/cm}^3)$$

Assume an exponential source distribution

$$S_v = S_v^0 e^{-\alpha z} \quad (2)$$

where

$$S_v^0 = \text{activity per unit volume at the surface } \left(\frac{\gamma/\text{sec}}{\text{cm}^3}\right)$$

$$\alpha = \text{reciprocal of the relaxation depth (cm}^{-1})$$

Rewrite Eq.1 in terms of  $\theta$  and  $z$ , combine with Eq.2 and integrate over  $z$ . Leads to

$$\phi = \frac{S_v^0}{2} \int_0^{\pi/2} \frac{\tan \theta \exp\left[-\mu/\rho)_a \rho_a h \sec \theta\right]}{\alpha + \mu/\rho)_s \rho_s \sec \theta} d\theta \quad (3)$$

Detector response defined in terms of an effective detector area, A, given by

$$A = \frac{N_p}{\phi} \quad (4)$$

where

$N_p$  = net photopeak count rate

The detector response, in general, varies as a function of the gamma ray angle of incidence and is normally written as

$$A = A_0 R(\theta) \quad (5)$$

where

$A_0$  = detector photopeak count rate for unit flux incident perpendicular to detector face

$$\left( \frac{\text{CPS}}{\gamma/\text{cm}^2 \text{ sec}} \right)$$

$R(\theta)$  = ratio of detector response at angle  $\theta$  to that at  $\theta = 0^\circ$

Determine  $A_0$  and  $R(\theta)$  experimentally for a given detector.

Combining Eq's 4 and 5 with Eq. 3 leads to an expression relating measured photopeak count rate to source activity in the soil.

$$\frac{N_p}{S_V^0} = \left[ \frac{A_0}{2} \int_0^{\pi/2} \frac{R(\theta) \tan \theta \exp[-\mu/\rho] a^{\rho_a} h \sec \theta}{\alpha + \mu/\rho) s \rho_s \sec \theta} d\theta \right] \quad (6)$$

in units of  $\frac{\text{cps}}{\gamma/\text{cm}^3\text{-sec}}$

Normally convert  $\gamma/\text{sec}$  to  $\mu\text{Ci}$  or  $\text{pCi}$  for a specific isotope. Can change from activity per unit volume to activity per unit mass by multiplying by the soil density ( $\text{g}/\text{cm}^3$ ).

For Enewetak want average concentration in top 3 cm. In general, average concentration in top  $z$  cm,  $S_V^z$ , is given by

$$S_V^z = \frac{1}{z} \int_0^z S_V^0 e^{-\alpha z} dz = \frac{S_V^0}{\alpha z} (1 - e^{-\alpha z}) \quad (7)$$

Combining Eq's 6 and 7 leads to the final expression for the conversion factor used at Enewetak

$$\frac{(S_V^z/\rho)}{N_p} = \frac{(1 - e^{-\alpha z})}{\alpha z} B \left[ \frac{A_0 \rho_s}{2} \int_0^{\pi/2} \frac{R(\theta) \tan \theta \exp[-\mu/\rho] a^{\rho_a} h \sec \theta}{\alpha + \mu/\rho) s \rho_s \sec \theta} d\theta \right]^{-1}$$

in units of  $\left[ \frac{\text{pCi/g}}{\text{cps}} \right]$

where  $B$  converts  $\gamma/\text{sec}$  to  $\text{pCi}$  for a specific isotope.

$^{241}\text{Am}$  INPUT PARAMETERS

$$h = 7.4\text{m}$$

$$\mu/\rho)_a = 0.188 \frac{\text{cm}^2}{\text{g}}$$

$$\rho_a = 1.15 (10^{-3}) \text{ g/cm}^3 \text{ (dry air at 750 mmHg and } 86^{\circ}\text{F)}$$

$$z = 3 \text{ cm}$$

$$A_o = 19.0 \frac{\text{cps}}{\gamma/\text{cm}^2\text{-sec}}$$

$$B = 75.3 \text{ } (\gamma/\text{dis.} = 35.9\%, \text{ pCi} = 3.7 \times 10^{-2} \text{ dis./sec})$$

R( $\theta$ ) = measured with collimator in place

Original

$$\mu/\rho)_s = 0.248 \frac{\text{cm}^2}{\text{g}}$$

$$\rho_s = 1.2 \text{ g/cm}^3$$

$\alpha$ : graphical analysis

Revised

$$\mu/\rho)_s = 0.333 \frac{\text{cm}^2}{\text{g}}$$

$$\rho_s = 1.5 \text{ g/cm}^3$$

$\alpha$ : weighted average  
from NVO-140

RESULTS

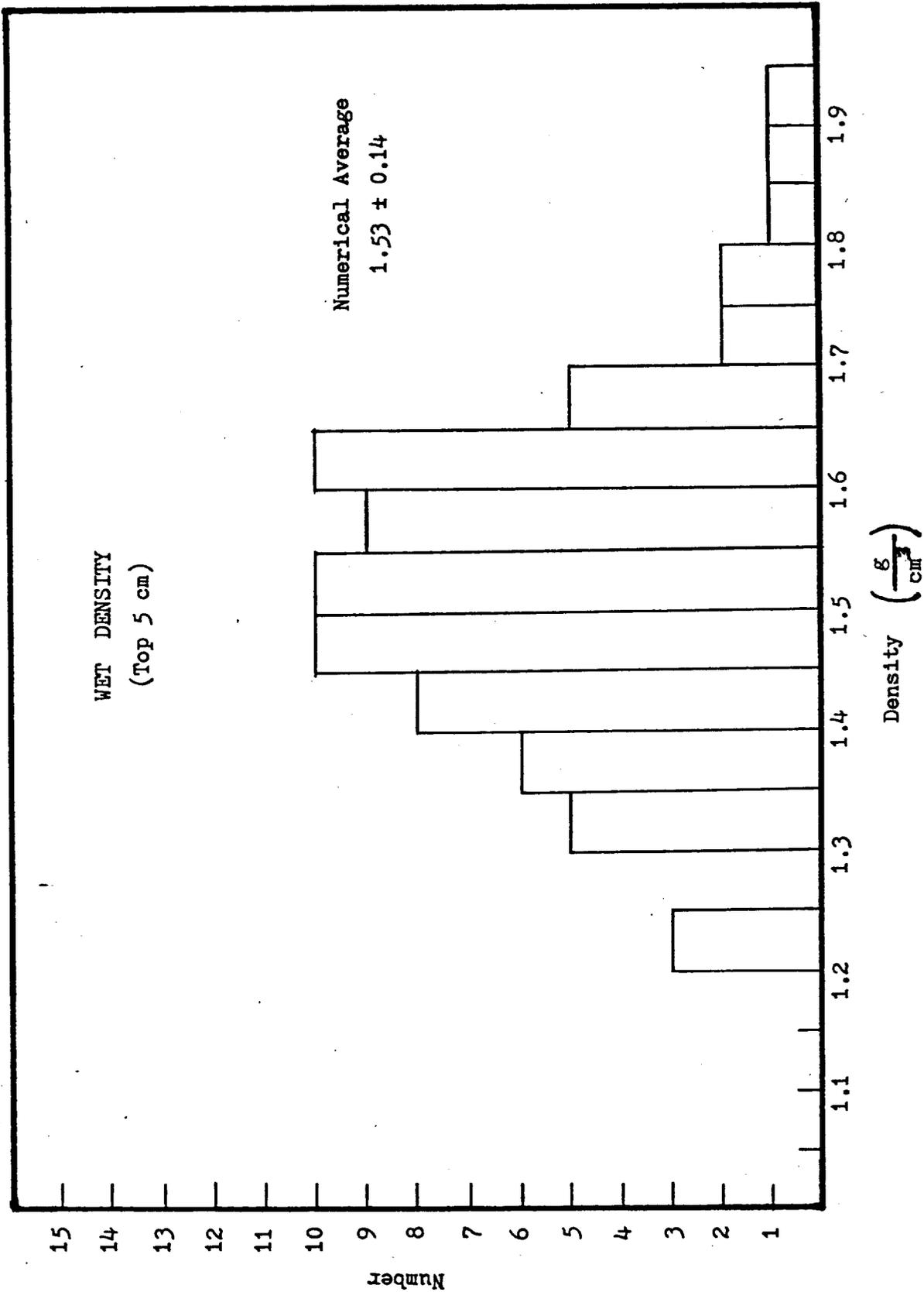
$$\frac{S_V^3/\rho}{N_p}$$

Original

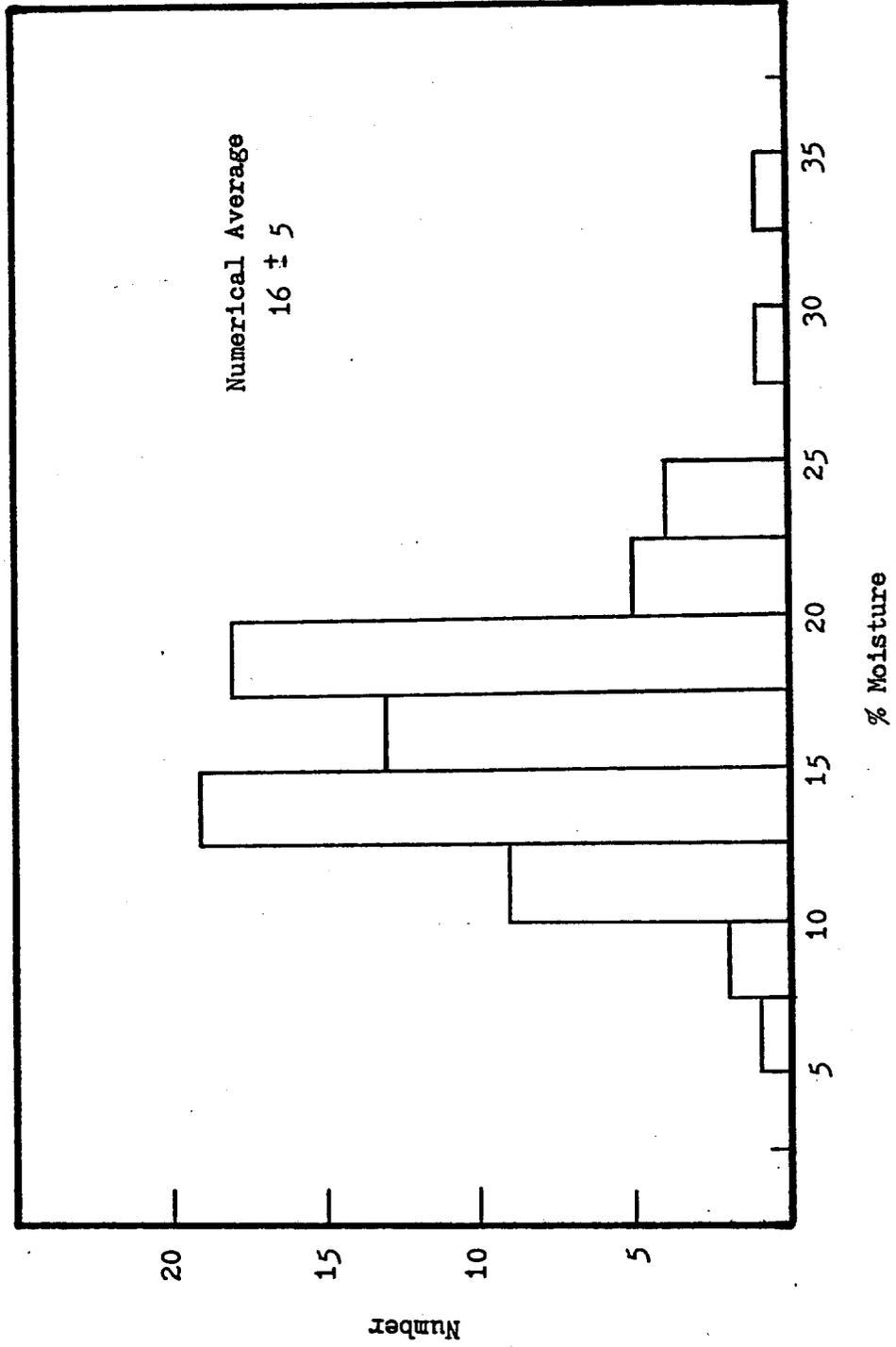
$$7.71 \frac{\text{pCi/g}}{\text{cps}}$$

Revised

$$8.95 \frac{\text{pCi/g}}{\text{cps}}$$



SOIL MOISTURE  
(Top 5 cm)



SAND CONE COMPARISON

	WET DENSITY		DRY DENSITY		% MOISTURE	
	Sand Cone	Troxler	Sand Cone	Troxler	Sand Cone	Troxler
1.	1.69	1.66	1.46	1.43	15.8	16.1
2.	1.64	1.71	1.43	1.46	14.7	17.1
3.	1.81	1.72	1.46	1.42	24.0	20.7
4.	1.60	1.63	1.37	1.35	16.8	20.7
5.	1.83	1.77	1.67	1.60	9.6	10.6
6.	1.57	1.46	1.22	1.30	28.7	12.3
7.	1.64	1.50	1.43	1.31	14.4	14.4
8.	1.68	1.61	1.41	1.41	19.1	14.2
9.	1.71	1.71	1.49	1.48	14.8	15.5
10.	1.68	1.59	1.43	1.36	17.0	16.9
11.	1.57	1.52	1.34	1.32	16.9	15.2
12.	1.66	1.77	1.47	1.55	12.8	13.8
Enewetak 1	1.86	1.73	1.68	1.56	10.7	10.9

Sand Cone  
Troxler

Wet 1.03 ± 0.05

Dry 1.02 ± 0.04

% 1.11 ± .39

w/o #6

1.02 ± 0.05

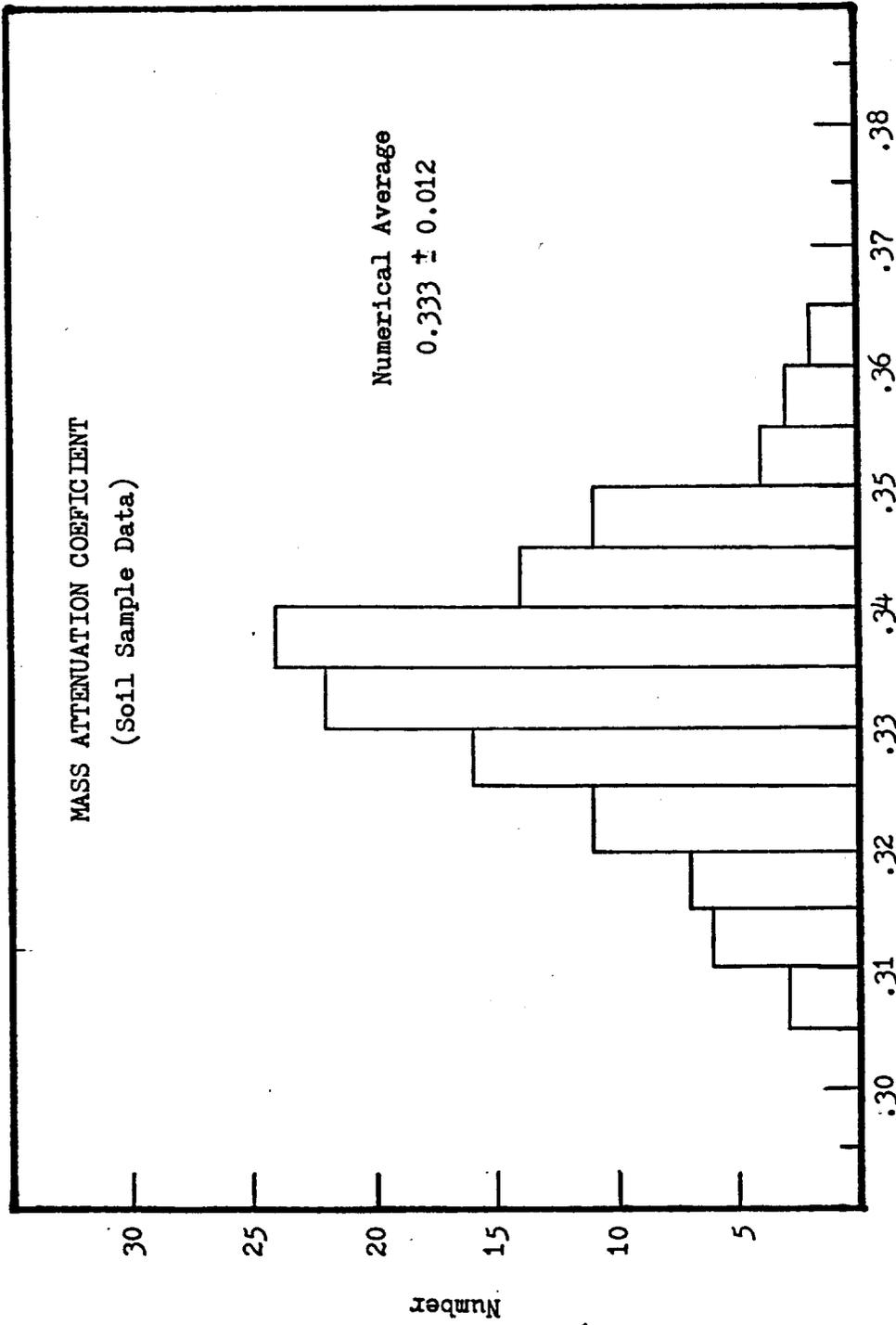
1.02 ± 0.04

1.00 ± 0.14

MASS ATTENUATION COEFFICIENT  
(Soil Sample Data)

Numerical Average  
 $0.333 \pm 0.012$

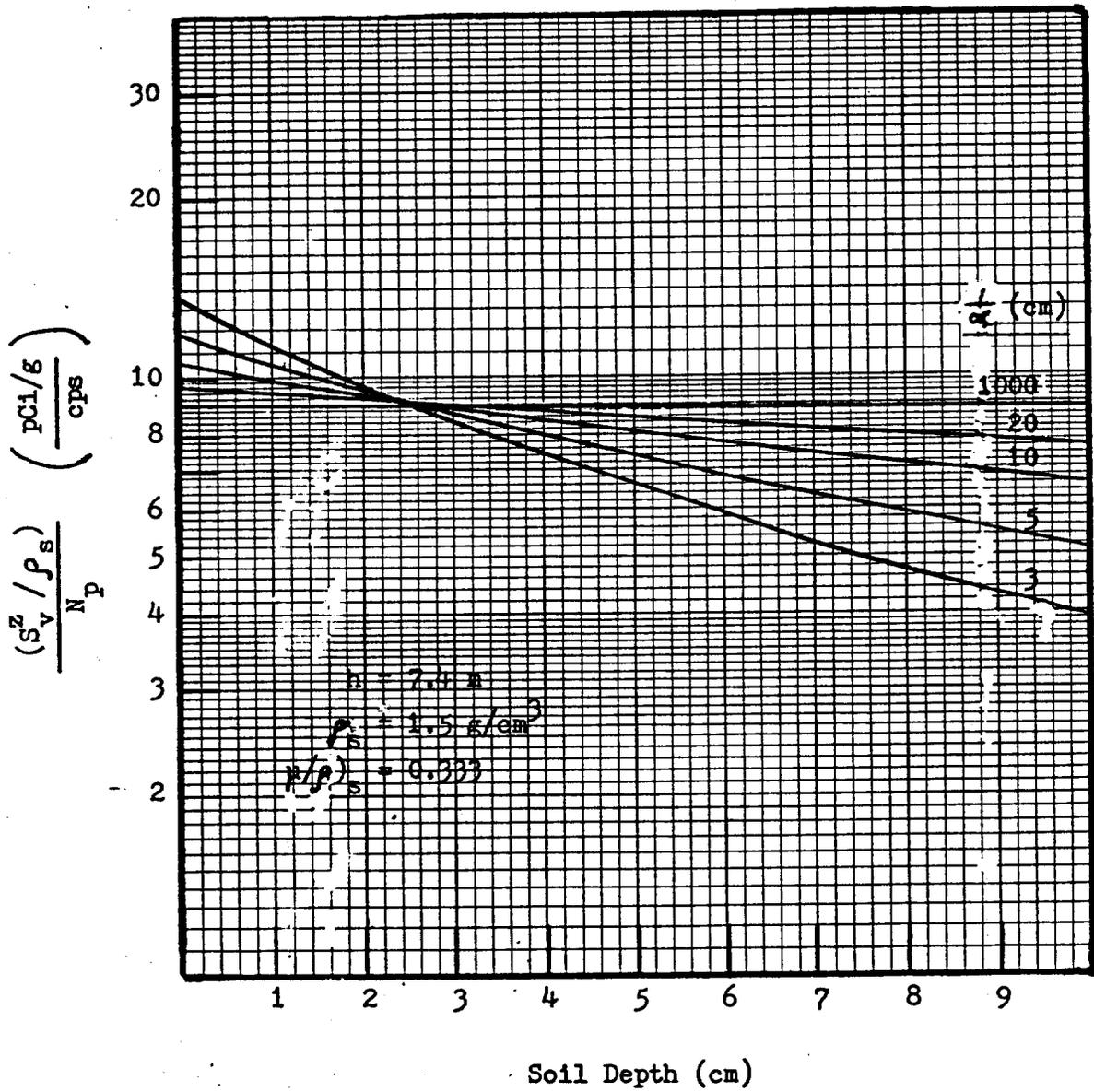
$$\frac{\mu}{\rho} \left( \frac{\text{cm}^2}{\text{g}} \right)$$



MASS ATTENUATION COEFFICIENTS

<u>SAMPLE</u>	<u>SOIL SAMPLE RESULTS</u>	<u>DIRECT MEASUREMENT</u>
1	0.330	0.337
2	0.324	0.320
3	0.331	0.339
4	0.322	0.328
5	0.342	0.342
6	0.340	0.338
7	0.332	0.335
8	0.336	0.337
9	0.327	0.322
10	0.333	0.333
11	0.335	0.329
Average	0.332	0.333
<u>Las Vegas</u>		
Commercial Dirt		0.273
Garden Dirt		0.279
-Desert Soil		0.246

# IMP CONVERSION FACTORS



REPOSITORY PNNL  
COLLECTION Marshall Islands  
BOX No. 5686  
FOLDER Miscellaneous Information

DOCUMENT DOES NOT CONTAIN ECI

Reviewed by H. Schuette Date 5/1/97